

A Lidar Approach to Measure CO₂ Concentrations from Space for the ASCENDS Mission

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ABSTRACT

We report on a lidar approach to measure atmospheric CO₂ column concentration being developed as a candidate for NASA's ASCENDS mission. It uses a pulsed dual-wavelength lidar measurement based on the integrated path differential absorption (IPDA) technique. We demonstrated the approach using the CO₂ measurement from aircraft in July and August 2009 over various locations. The results show clear CO₂ line shape and absorption signals, which follow the expected changes with aircraft altitude from 3 to 13 km. The column absorption measurements show altitude dependence in good agreement with column number density estimates calculated from airborne in-situ measurements. The approaches for O₂ measurements and for scaling the technique to space are discussed.

1. INTRODUCTION

Although increasing atmospheric CO₂ is widely accepted as the largest anthropogenic factor causing climate change, there is considerable uncertainty about its global budget. Accurate measurements of tropospheric CO₂ mixing ratios are needed to study CO₂ emissions and CO₂ exchange with the land and oceans. To be useful in reducing uncertainties about carbon sources and sinks the atmospheric CO₂ measurements need deg-level spatial resolution and ~ 0.3% precision [1,2]. Several groups have analyzed the potential of space missions using passive spectrometers [3-5], and the GOSAT mission [6] is now making global CO₂ measurements from space using an FTIR spectrometer and surface reflected sunlight. However sun angle limitations restrict its measurements to the daytime and mid-latitudes. An inherent error source with space-based passive spectrometers is optical scattering from thin clouds, particularly cirrus, in the measurement path [7,8]. Optical scattering in the measurement path modifies the optical path length and thus the total CO₂ absorption viewed by passive spectrometers. It can cause large retrieval errors even for thin cirrus clouds [9].

To address these limitations, the US National Research Council's 2007 Decadal Survey for Earth Science recommended a new space-based CO₂ measuring mission called ASCENDS [10]. Its goals are to produce global atmospheric CO₂ measurements using the laser absorption spectroscopy measurement approach. The mission's goals are to quantify global spatial distribution of atmospheric CO₂ with 1-2 ppm accuracy, and quantify the global spatial distribution of terrestrial and oceanic sources and sinks of CO₂ on 1-degree grids with approximately monthly time resolution. The ASCENDS approach offers continuous measurements over the cloud-free oceans, at low sun angles and in darkness, which are major advantages over passive sensors. ASCENDS mission organizers held a workshop in 2008 to better define the science and measurement needs and planning for future work [11]. ESA has also conducted mission definition studies for a similar space mission called A-SCOPE [12,13]. The lidar sensitivity and spectroscopic analyses performed as part of the A-SCOPE definition activities have been recently published [14,15].

2. LIDAR APPROACH

Several groups have measured atmospheric CO₂ absorption using DIAL lidar techniques. A summary of these has been recently published [16]. Our group has been developing a pulsed lidar approach as a candidate for the

ASCENDS mission [17-19]. The approach, shown in Figure 1, uses a dual band pulsed laser absorption spectrometer and the integrated path differential absorption (IPDA) lidar technique. The approach uses two tunable pulsed laser transmitters allowing simultaneous measurement of the absorption from a CO₂ absorption line in the 1570 nm band, O₂ extinction in the oxygen A-band, and surface height and atmospheric backscatter in the same path. A tunable laser is stepped in wavelength across a single CO₂ line for the CO₂ column measurement, while simultaneously a laser is stepped across a line doublet near 765 nm in the Oxygen A-band for an atmospheric pressure measurement [20, 21]. Both lasers are pulsed at a ~8kHz rate, and the two absorption line regions are sampled in wavelength steps at typically ~1 KHz. Both laser transmitters utilize tunable diode lasers followed by laser amplifiers. The direct detection receiver measures the time resolved laser backscatter from the atmosphere along with the energies of the laser echoes from the surface. After suitable averaging the gas extinction and column densities for the CO₂ and O₂ gases are estimated from the sampled wavelengths of the surface reflected line shapes via the Differential Absorption Lidar (DIAL) technique [22].

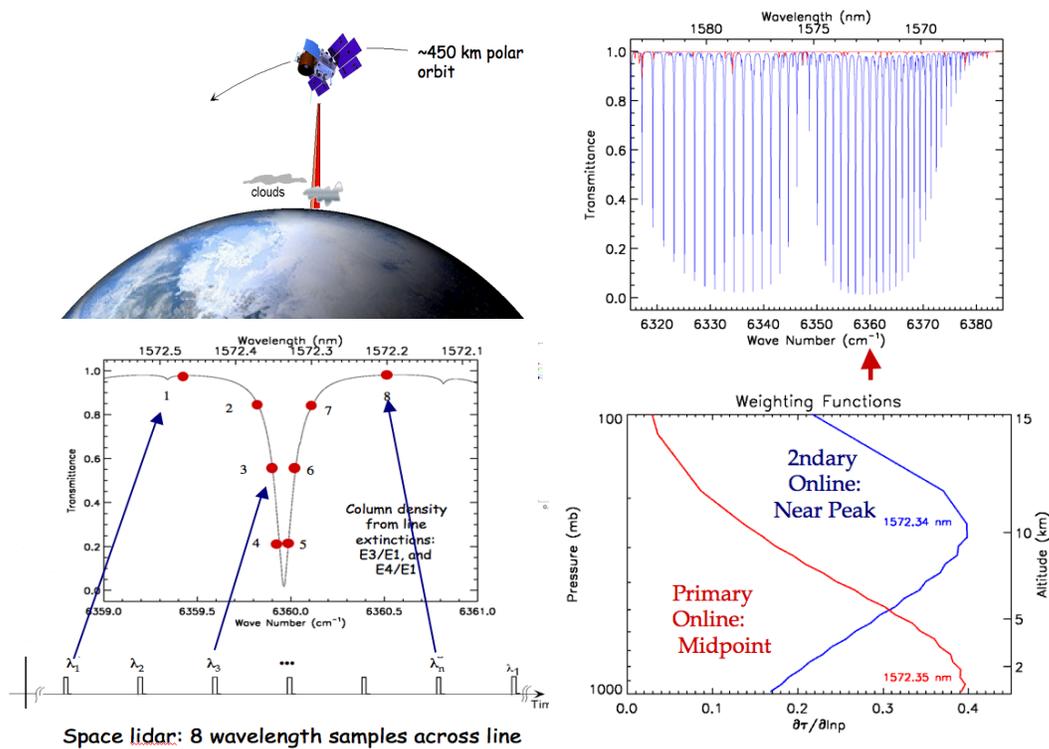


Figure 1 – *Top Left* – Space measurement concept. *Top right* - 2-way transmission for the 1570 nm CO₂ band from space computed from HITRAN 2004. The technique measures the absorption of a single line in this band. *Bottom Left*- The present selection of the 1572.33 nm CO₂ line, and wavelength sampling strategy for space. *Bottom Right* – The computed weighting functions for the space measurement using the ratio of the mid-point wavelengths (points 3 and 6) to offline ratio (in red) and the near peak (points 4 and 5) to offline ratio (in blue). The red curve shows the nearly uniform tropospheric vertical weighting function which is needed for the ASCENDS flux determinations.

The approach is flexible, and the concept for space measures the CO₂ lineshape at 8 wavelengths. This provides several capabilities and allows using vertical atmospheric weighting functions at 2 heights [23]. Sampling at multiple wavelengths across the absorption line allows for solving for wavelength offsets via a line fitting process. The distributed wavelength sampling across the line region also allows the instrument's response to be characterized as a function of wavelength. These capabilities allow modeling and reducing the impacts of wavelength dependent responses in the lidar. Using pulsed lasers and receiver processing to time (and height) resolve the laser backscatter profiles also allows post detection signal processing to isolate the laser echo signals from the surface, and to reject laser photons scattered from the atmosphere which arrive earlier. Hence it allows isolating the full column measurement from bias errors caused by atmospheric scattering [7,8]. Isolating the surface echo with a time gate in

receiver processing also substantially improves the receiver's signal-to-noise ratio by reducing the amount of noise from the detector and the solar background.

3. CO₂ SPECTROSCOPY AND LINE CHOICE

We use a single line in the 1570 nm band (Fig. 1) for the CO₂ measurement [7]. This vibration-rotation band of CO₂ has an appropriate range of absorption that provides good sensitivity to the surface echo signal and to variation in CO₂ in the lower troposphere. This band has minimal interference from other atmospheric species like H₂O, and has several different temperature insensitive lines. The shorter wavelength lines in the R-branch are a better match to available laser and detector technologies. The centermost line of R-branch at 1572.335 nm, shown in Figure 1, has been analyzed and appears as an attractive line for CO₂ measurements [23]. It has the minimum temperature sensitivity, particularly to the lower atmospheric temperature changes. It also provides the maximum CO₂ absorption in the R-branch. Absorption measurements on this line at different wavelengths yield the line shape and CO₂ vertical column densities with weighting functions peaking at different altitudes.

4. PULSED IPDA MEASUREMENT APPROACH

The IPDA technique is a well-established lidar technique for open-path laser absorption spectroscopy measurements [22,24]. It is essentially a special case of differential absorption lidar, where a scattering target (such as the ground, a water surface, or cloud tops) is used at the end of the path. Typically two laser wavelengths are used, and the target is illuminated with the laser alternatively tuned onto the gas absorption line, and off it. The path-integrated gas absorption attenuates the on-line laser energy relative to the off-line wavelength. By measuring the optical depth of the gas absorption line and range, and by knowing the difference in gas absorption cross-sections, one can solve for the path integrated gas number density. In our lidar the photon counting receiver records and accumulates the time resolved backscattered photon counting profiles for the wavelength steps across the line for a given integration time. This allows recording the cumulative laser backscatter profile at each transmitted wavelength. This contains time resolved atmospheric backscatter as well as the surface echo pulses at each wavelength. The absorption line shape and optical depth are computed from the echo pulse energies, usually at the longest range at the end of the path.

The error of the lidar measurement of optical depth and path integrated number density depends on its signal and noise characteristics and the magnitude of bias errors. A detailed analysis must account for many factors, including variability in the lidar parameters, atmospheric temperature and pressure, turbulence, laser speckle, changing surface reflectivity and range, etc. [14,15]. A simplified treatment for this approach, for an open atmospheric path and target at a fixed range R, illustrates most of the important dependencies, and is given in [16].

5. AIRBORNE LIDAR DESCRIPTION

In 2007, we demonstrated ground-based lidar [25] measurements of column CO₂ absorption in horizontal paths. In 2008 we adapted the lidar for use on the NASA Glenn Lear-25 aircraft [26] shown in Figure 2. A block diagram of the flight instrument is shown in Figure 3. Modifications to the ground-based lidar included converting the laser transmitter to pulsed operation by adding an acousto-optic modulator (AOM) between the diode laser and the fiber amplifier, removing the chopper wheel, and improving the receiver sensitivity by using a PMT detector, followed by a discriminator and multi-channel scaler (MCS). The airborne lidar specifications are listed in Table 1.



Figure 2- *Left* - NASA Glenn Lear-25 aircraft. The nadir window assembly is just below the NASA logo. Photographs of the lidar installed on the aircraft showing the sensor head assembly (*Middle*) and the dual aircraft racks (*Right*).

Table 1 – 2009 Pulsed Airborne CO₂ Lidar Parameters

CO ₂ line center wavelength	1572.33 nm (typically)	Telescope diameter	20 cm
Laser min & max wavelengths	1572.29 nm, 1572.39 nm	Receiver FOV diameter	200 μrad
Laser wavelength steps across line	20 (these flights)	Receiver optical bandwidth	800 pm FWHM
Laser wavelength change/step	~ 5 pm	Receiver Optics Transmission	64%
Laser peak power, pulse width, energy	25 watts, 1 μsec, 25 μJ	Detector PMT type	Hamamatsu H10330A-75
Laser divergence angle	100 μrad (these flights)	Detector quantum efficiency	2% (this device)
Seed laser diode type	DFB: Fitel FOL15DCWD	Detector dark count rate	~ 500 kHz
Laser Pulse Modulator (AOM)	NEOS Model: 26035-2-155	Receiver signal processing	Photon counting/histogramming
Fiber coupled CO ₂ cell	80 cm path, ~200 Torr pressure	Histogram time bin width	8 nsec
Fiber Laser Amplifier (EDFA)	IPG EAR-10K-1571-LP-SF	Receiver integration time	1 second per readout
Laser line scan rate	450 Hz	Recording duty cycle	50% (1 sec. every 2 sec.)
Laser linewidth per step	~15 MHz	Instrument rack size & mass:	~ 90 cm tall, total: 147 kg
Receiver Telescope type	Cassegrain, f/10 (Vixen)	Sensor head size and mass	~ 25 x 60 x 60 cm, 41 kg

A laser signal drawing and lidar block diagram are shown in Figure 3. The lidar signal source is a DFB laser diode, which is operated near 1572.33 nm by controlling its temperature and current. A ramp from a signal generator was used to sweep the current to the diode laser, and hence its output wavelength. The diode's CW output is then gated into pulses using an acousto-optic modulator (AOM) to an Erbium Doped Fiber Amplifier (EDFA). A small percentage of the CW seed laser output is split off and directed through a fiber-coupled CO₂ absorption cell and to a PIN detector. The CO₂ cell serves as a monitor for center wavelength of the sweep. The nominal static transmitted laser pulse wavelengths are measured in a calibration procedure using a commercial wavemeter. Subsequent testing showed some curvature in the scanning dynamic ramp signal, so we used a more accurate quadratic functional model for the laser wavelength vs pulse position in the data analysis.

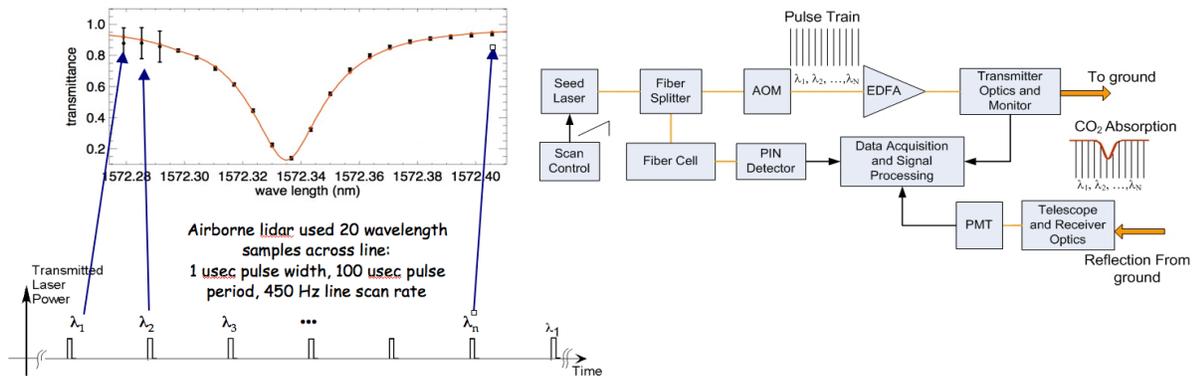
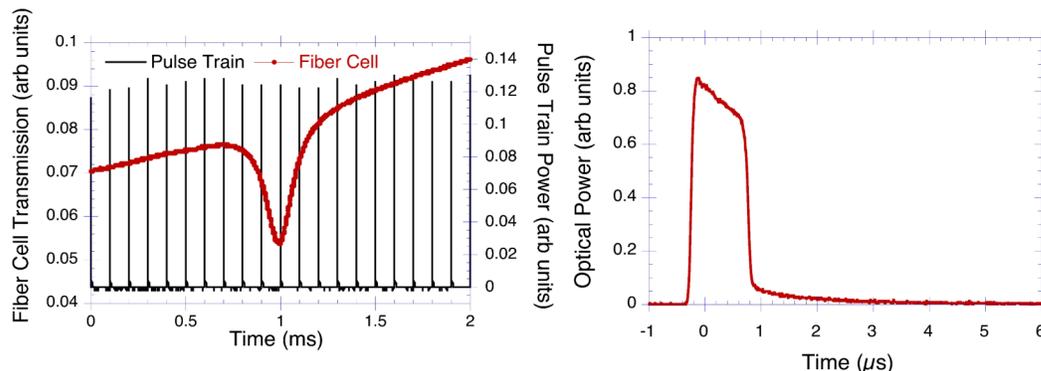


Figure 3. *Left* – CO₂ Line sampling approach for airborne lidar. *Right* – CO₂ lidar channel block diagram.

The laser output is a sequence of 1 usec-wide laser pulses, shown in Figure 4, which occur at a 10 KHz rate. A sample of the laser diode sweep through the internal cell containing CO₂ is shown with a sample of the pulsed transmitter wavelength sweep, along with the optical power vs time waveform of a single pulse from the transmitter. The collimated transmitted laser signal exits through nadir aircraft window. The laser backscatter is collected by the receiver's 20 cm diameter Cassegrain telescope, which views nadir through the same window in a bistatic configuration. A multimode fiber is used to couple the optical signal from the telescope focal plane to the receiver optics. After passing through an optical bandpass filter, the signal is focused onto a PMT detector. The PMT used in the 2009 flights had a single photon counting efficiency of ~2%. The electrical pulse output from the PMT was amplified and passed through a threshold detector.

The pulses from the receiver's PMT detector and discriminator are binned and accumulated by the MCS. The start time of the MCS sweep is synchronized with the first laser pulse trigger and hence start of the pulsed wavelength sweep. Each MCS sweep contains a histogram of PMT pulse counts vs time for the wavelength sweeps (i.e. the laser backscatter profiles for all 20 pulses). At the end of 1 second, each bin contains the total receiver counts for the 450 laser sweeps. The receiver histogram record is then read and stored. The laser trigger and data acquisition is synchronized to timing markers from the GPS receiver and data was stored every other second. The computer also

digitizes other signals, including those from thermocouples distributed across the sensor head and electronic rack, the inertial guidance system output from the aircraft and GPS position and time. A nadir viewing video camera also records the visible image through the window.



Figures 4. *Left* – Example of the laser wavelength scan. (red trace and left hand axis) - Sample cw wavelength scan of the diode laser (before the modulator) through the instrument’s internal pressure CO₂ cell, showing CO₂ absorption and diode laser power variability vs wavelength. (Black trace and right hand axis) – Detected laser output power vs time from the laser transmitter’s power monitor. *Right* - Typical single laser pulse (in red, left hand axis) from the airborne laser transmitter. The pulse shape shows decay as the fiber amplifier gain is depleted. The 1usec wide part of the laser pulse contains over 90 % of the pulse energy.

7. 2009 AIRBORNE CAMPAIGNS

We used the NASA Glenn Lear-25 aircraft [26] for these flights. The airborne lidar is configured into two half-racks and a “sensor head”, which contained the receiver telescope and the transmitter optics. A photograph of the sensor when integrated on the aircraft is shown in Figure 2. The sensor head was mounted above the aircraft’s nadir viewing window. For the 2009 flights a pair of wedged and anti-reflection coated optical windows were used in the aircraft’s nadir window assembly.

During late-July though mid-August 2009 we flew an airborne campaign with a series of 2.5 hour-long flights. We measured the shapes of the atmospheric CO₂ absorption line at stepped altitudes from 3-13 km over a variety of surfaces in Nebraska, Illinois, the SGP ARM site, and near and over the Chesapeake Bay in North Carolina and eastern Virginia. Strong laser signals and clear CO₂ line shapes were observed at all altitudes on most flights, and some measurements were made through thin and broken clouds. These flights allowed testing and recording performance under different measurement conditions. These included measuring to the ground through broken and thin clouds. An example of these measurements is shown in Figure 5.

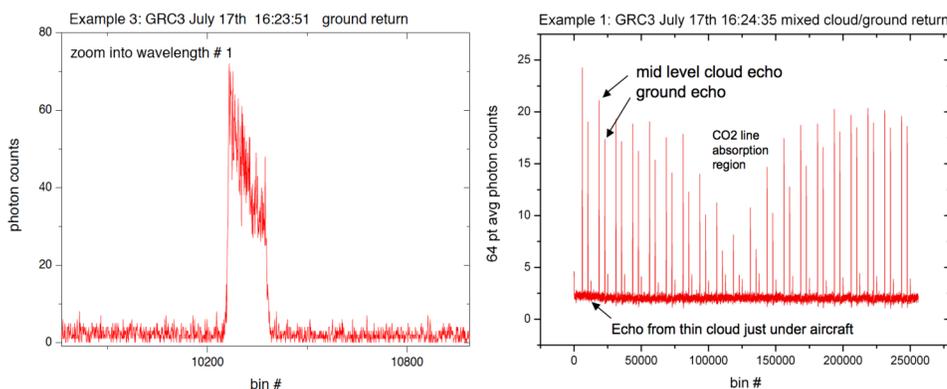


Figure 5. *Left* - A typical single accumulated pulse shape measured from the ground echoes from the photon counting receiver. *Right* - Example of a raw (uncorrected) recorded backscatter profile when measuring to the ground through 2 thin cloud layers. It shows 3 time displaced echo pulses per transmitted pulse. The smallest initial echo pulses are from the cirrus clouds just under the aircraft. The figure also shows the two range displaced CO₂ column absorptions which are evident in the echoes from the mid-level cloud layer and the deepest absorption in the longest path to the ground.

The figure shows the time resolved triple-echo pulses measured when viewing the ground over Ohio through two thin clouds layers. The first pulse in each triplet is the reflection from the cirrus cloud, while the second is reflection from the mid altitude cloud and the third from the ground. The different amounts of CO₂ column absorption for the different path lengths are evident. Without a range resolved receiver, the echo pulse signals and measurements from the three different path lengths would be mixed. Using the pulsed measurement approach allows using range gating in the data processing to isolate the signals from the surface and hence eliminates optical path length errors from atmospheric scattering.

8. AIRBORNE CO₂ MEASUREMENTS AND CALCULATIONS

In order to estimate the actual CO₂ column density during the flights, measurements of atmospheric temperature, moisture and pressure vertical profiles were used from the radiosonde balloons, which were launched near the flight location. Their parameters were used in a 40 layer atmospheric model to compute dry air column density vs height to 13 km altitude. The airborne flights were also coordinated with LaRC investigators, and the flights over the ARM site, NC and VA were under-flown with in-situ gas measurements made from the NASA LaRC UC-12 aircraft. This used a quick-response infrared absorption gas analyzer to measure CO₂ concentrations. It sampled air and CO₂ concentrations every second from takeoff to the aircraft's upper flight altitude and back to the ground.

The AVOCET (Atmospheric Vertical Observation of CO₂ in the Earth's Troposphere) *in-situ* CO₂ measurement system [28,29] was used to obtain high-precision, high-accuracy measurements of CO₂ mixing ratios profiles under the flight track of the GSFC CO₂ Sounder during the flights over Oklahoma, North Carolina and Virginia. AVOCET uses a modified LI-COR model 6252 non-dispersive infrared (NDIR) gas analyzer-based sampling system with dual sample cells to achieve high CO₂ measurement precision by comparing the differential absorption between the sampled air and a calibrated reference gas that is traceable to the World Meteorological Organization primary calibration standards maintained at the National Oceanic and Atmospheric Administration, Climate Monitoring and Diagnostics Laboratory in Boulder, Colorado. During ambient sampling, air was continuously drawn through a Rosemount probe, a permeable membrane dryer to remove H₂O_(v), the LI-COR analyzer, and then through the diaphragm pump. Frequent but short calibrations with well-documented and stable calibration gases, critical to achieving both high precision and accuracy, were accomplished by periodically (~15 minutes) flowing calibration gas through the instrument's sample cell. The system was operated at a constant mass flow rate (500 cm³ min⁻¹) and pressure (250 torr), and had a CO₂ measurement precision of ≤ 0.1 ppm ($\pm 1\sigma$) and accuracy of ± 0.25 ppm for 1 Hz sampling rates. AVOCET CO₂ measurements were made from a maximum altitude of 8 km to below 300 m AGL (above ground level). In the case, when the spiral was done over a "low-use" airport, the *in situ* measurements were done down to the ground in a "touch and go" of the airport runway. All AVOCET measurements were integrated with GPS latitude, longitude, and altitude measurements made on the UC-12. The spirals were timed to coincide with over-flights of the GSFC CO₂ sounder. The line shape, averaged 2-way optical depth for the 1572.335 nm line, and the CO₂ column number density were computed versus flight altitude based on these readings. These calculations provided a reference comparison for the airborne lidar measurements and showed how the CO₂ line shapes and depths should vary with flight altitude.

Vaisala RS-92 radiosondes were also launched during each test flight to obtain the meteorological parameters needed for converting the CO₂ mixing ratios measured by AVOCET to the path integrated CO₂ column density needed to compare with the lidar. The RS-92 radiosondes have a pressure, temperature, and relative humidity absolute accuracies from 1080-100 hPa of 1 hPa, 0.5 °C, and 5%, respectively. These radiosondes were launched from the ground at the center of the UC-12 spiral location, and when possible, they were launched at the completion of the UC-12 spiral. Close coordination was maintained between the UC-12, Lear-25, and ground radiosonde personnel to ensure the most coincident data acquisition for comparison of the remote and in situ-derived CO₂ data.

9. 2009 CO₂ MEASUREMENT PROCESSING

For the flights the lidar recorded the time- and wavelength-resolved laser backscatter with 1 second integration time. In subsequent analysis, the line shape measurements at each flight altitude step were averaged. We used a CO₂ line retrieval approach based on the Gauss-Newton method [30] to analyze each altitude averaged line shape. This approach has sufficient free parameters to model and correct for instrument effects, to fit the resulting CO₂ line shapes, and to estimate the corresponding CO₂ column densities and optical depth at each altitude. The CO₂ retrieval

algorithm yields an estimate of the mean CO₂ column density over the laser path length based on line absorption strength taken from the HITRAN 2004 database. The input observations were the ratio of the photon counts in the surface echo signals at each wavelength after they were normalized by an estimate of transmitted pulse energy. The error covariance matrix for the observed signals was diagonal and equally weighted for all but the first three wavelengths. Examples of calculated and the observed (retrieved) line shapes for the 8/4/09 flight over the ARM site and the 8/17/09 flight over North Carolina are shown in Figures 6 and 7.

The algorithm requires several other inputs. First are estimates of the vertical profile of temperature, pressure and water vapor versus altitude. These are used to calculate the approximate CO₂ line shape, and were estimated from gridded meteorological fields from the Goddard Modeling and Assimilation Office for the locations at the time of the flights. They are used to calculate the wavelength resolved absorption spectra of atmospheric CO₂ based upon HITRAN 2004 for each 1 km altitude bin. The algorithm also uses the path length from the aircraft to the surface, which was calculated from the laser pulse's time of flight. Based on both ground-based testing and subsequent airborne measurements, the range resolution for these flights was estimated to be < 5m. Since this was ~0.2% or less of the column height, its contribution to the overall CO₂ measurement error was negligible.

The algorithm attempts to fit the sampled CO₂ line shape using a model with several sets of variables. The first is the reduction of the photon count ratio near the 1572.335 nm line due to CO₂ absorption. Since the photon counts for the line shape samples are measured as a function of pulse number, they are converted to wavelength before comparing the observed spectra with the HITRAN data. For these experiments the lidar's wavelength (ie wavelength per laser pulse number) was modeled as a quadratic function, and the three wavelength coefficients were solved for, using the ground calibration as a prior constraint. The final set of variables modeled the changes in the lidar's baseline response with wavelength. This product can change during flight due to the changing physical environment of the lidar. We fit (modeled) and normalized for an estimate of the baseline variability using a quadratic energy dependence with pulse number.

The CO₂ column results are being analyzed by flight location. The measured CO₂ column density vs altitude plots in Figures 6 and 7 were computed from the in-situ sensor readings from the LaRC aircraft (red line, lower x-axis). Other analysis of the 2009 flights showed that the average signal levels follow predicted values [31], and that the altimetry measurements over water had an uncertainty of ~3 m [32]. Although the CO₂ absorption analysis is continuing, the preliminary agreement on these flights between the estimated optical depths from the lidar, and the computed ones is quite good.

10. OXYGEN ABSORPTION MEASUREMENT

In order to accurately estimate the CO₂ mixing ratio, the ASCENDS mission requires a measurement of the dry air column density simultaneously with the CO₂ column. Our group is also developing a lidar approach to measure atmospheric pressure in the same path by adding a parallel lidar channel with measures column absorption of a line pair in the O₂ A-band [20, 21]. We have developed a breadboard lidar for O₂, and measured its column absorption from the laboratory over an outdoor horizontal path using the instrument shown in Figure 8. In July 2010 we demonstrated airborne measurements of O₂ column absorption using this approach. These results will be reported in the future.

11. SCALING TO SPACE

A space-based version of this lidar must have a much larger lidar power-area product due to the ~x40 longer range and faster along track velocity. We have developed receiver SNR models for both the CO₂ and O₂ channels and applied them to estimate lidar parameters needed for the space measurement. Some initial calculations used to estimate the needed laser energies for a space are shown in Figure 9. These are for a 500 km orbit, a 1.5 m diameter telescope and a 10 second integration time, which allows a 70 km along track integration in low earth orbit. The received SNR and relative measurement error are plotted versus laser peak power for a 1-usec wide laser pulse in Figure 9. The calculations show that ~3 mJ laser energies are required to attain the precision needed for each measurement. These calculations are conservative by 3 dB since they assume that only single on- and off-line measurements are made, where our approach uses twice as many measurements.

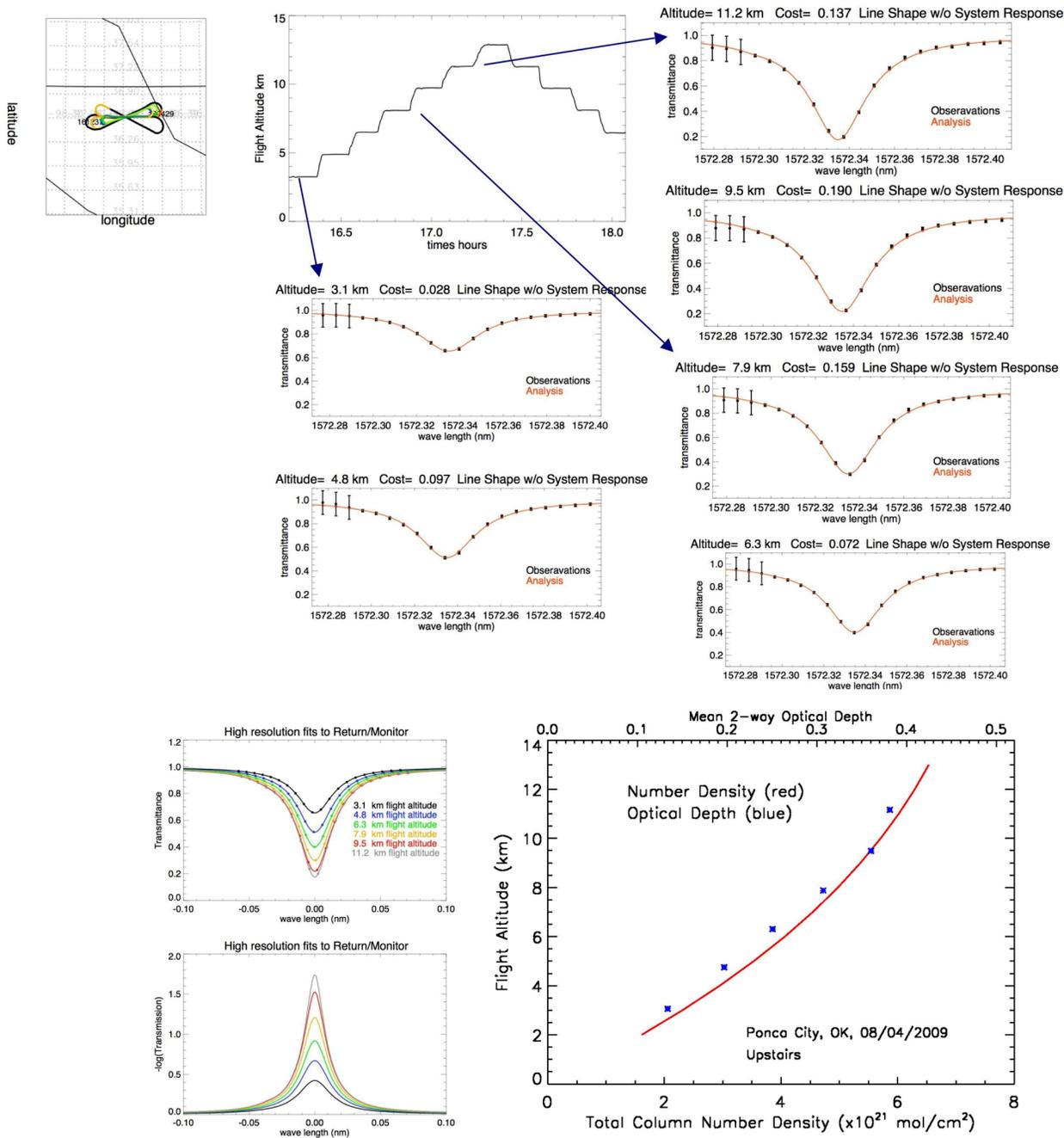
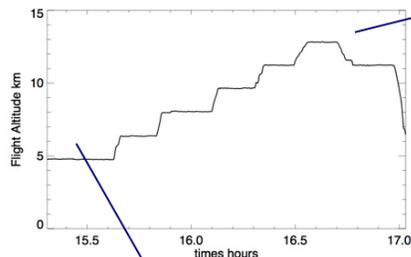
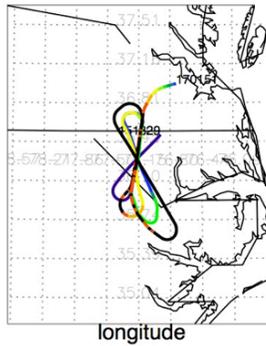
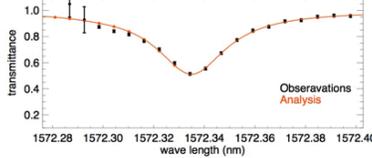


Figure 6- Top – *Top set* - Outline of the flight pattern and sample measurements of the 1572.33 nm CO₂ line for flight above the DOE SGP ARM site on 8/4/09. *Left* – map of location of “bowtie” flight patterns. The altitude changes in curved part of one bowtie, *Center top* – Altitude history of flight, showing aircraft altitude steps from 3.1 to 11.2 km, *Other upper plots* – measured CO₂ absorption line shapes (black dots) at the constant altitude steps given and orange lines showing CO₂ line shape fits through the measurements. *Bottom plots* - Initial analysis of the 1572.33 nm CO₂ shape measurements for this flight. – Overlaid plot of the fitted CO₂ line transmission vs wavelengths, from Figure 4, for the altitudes indicated. *Bottom Left* – Computed CO₂ optical depths vs wavelength from the optical transmissions. *Right*– plot of measured CO₂ absorption mean optical depths (in blue, for upper x-axis), vs altitude. The measured CO₂ column density vs altitude computed from the in-situ sensor readings from the LaRC aircraft (red line, for lower x-axis). There was a smooth increase in measured optical depth, except for the measurement at 9.5 km altitude.

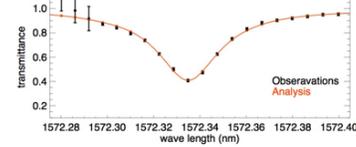
Examples of Line shapes vs Altitude
North Carolina
Flight - August 17,
2009



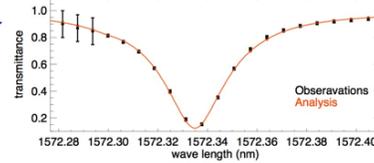
Altitude= 4.9 km Cost= 2.614 Line Shape w/o System Response



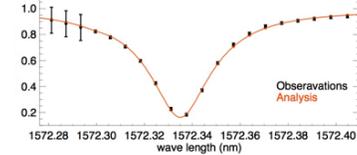
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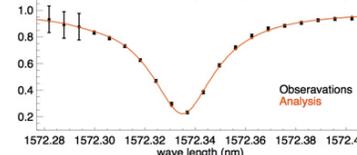
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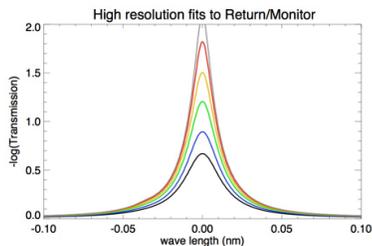
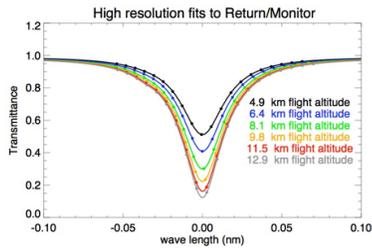
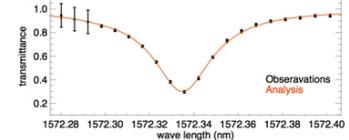
Altitude= 11.5 km Cost= 0.155 Line Shape w/o System Response



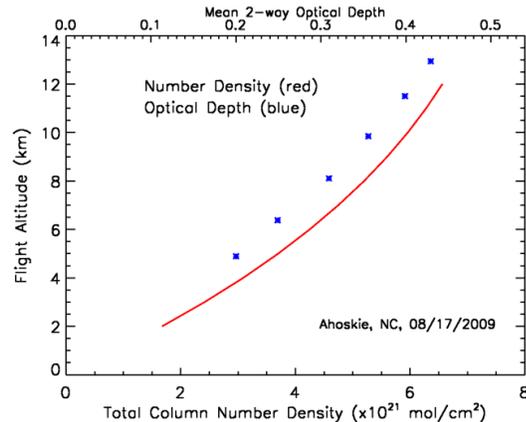
Altitude= 9.8 km Cost= 0.181 Line Shape w/o System Response



Altitude= 8.1 km Cost= 0.117 Line Shape w/o System Response



Line Optical Density & # Density vs Altitude
North Carolina Flight - August 17, 2009



- Mean Optical Depths (blue) from line fits to CO₂ Sounder measurements
- # Densities calculated (red line) from LaRC in-situ sensor and radiosonde readings

Figure 7- Top – Top set – Outline of the flight pattern and sample measurements of the 1572.33 nm CO₂ line for flight above North Carolina on 8/17/09. Left – map of location of “bowtie” flight patterns. The altitude changes in curved part of one bowtie, Center top – Altitude history of flight, showing aircraft altitude steps from 4.9 to 12.9 km, Other upper plots – measured CO₂ absorption line shapes (black dots) at the constant altitude steps given and orange lines showing CO₂ line shape fits through the measurements. Bottom plots - Initial analysis of the 1572.33 nm CO₂ shape measurements for this flight. – Overlaid plot of the fitted CO₂ line transmission vs wavelengths, from Figure 4, for the altitudes indicated. Bottom Left – Computed CO₂ optical depths vs wavelength from the optical transmissions. Right – plot of measured CO₂ absorption mean optical depths (in blue, for upper x-axis), vs altitude. The measured CO₂ column density vs altitude computed from the in-situ sensor readings from the LaRC aircraft (red line, for lower x-axis). There was a smooth increase in measured optical depths vs altitude, which matched the calculated trend.

Based on these SNR and laser energy estimates the Goddard Instrument Development Laboratory has conducted two space lidar design studies for ASCENDS. The instrument concept drawing from the first study is shown in Figure 9.

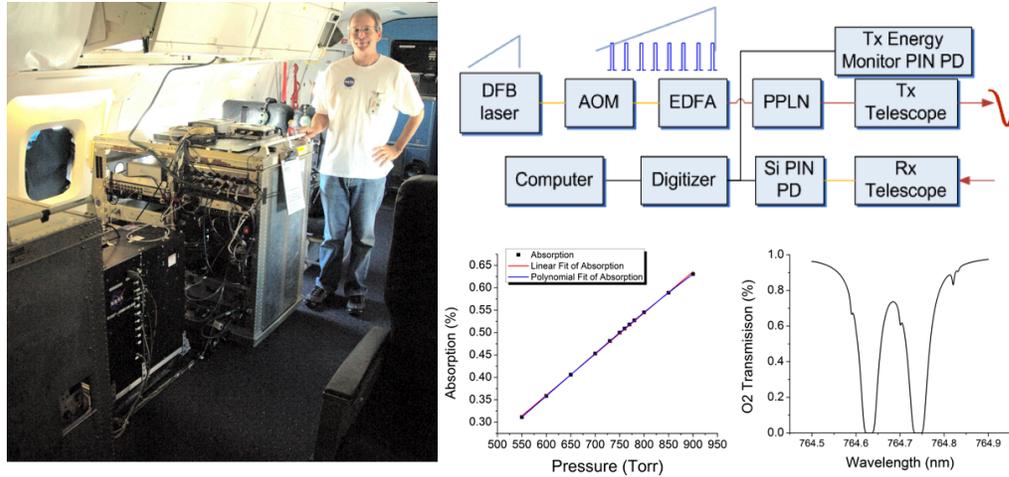


Figure 8- Oxygen lidar measurement channel. *Left*- Photograph of the combined CO₂ and O₂ lidar flown in July 2010 on the NASA DC-8 with Randy Kawa. – *Top right* – O₂ lidar channel block diagram, where the receiver telescope is shared with the CO₂ channel. Some parameters of the breadboard O₂ lidar are: Diode laser wavelength: 1529-1530 nm, Laser amplifier: NP Photonics EDFA, Lidar measurement wavelength: 764.5 – 764.9 nm, Laser pulse energy: ~2 uJ/pulse, laser pulse width: 250 nsec, Laser pulse rate: 10 KHz Number of wavelength steps: 40, Detector type: Si APD (SPCM). *Bottom middle* – Calculation showing nearly linear dependence of the absorption of the valley between the two O₂ lines with surface pressure. *Bottom right* - Calculated absorption for the O₂ line doublet vs wavelength for a horizontal path with a target at 1.5 km range.

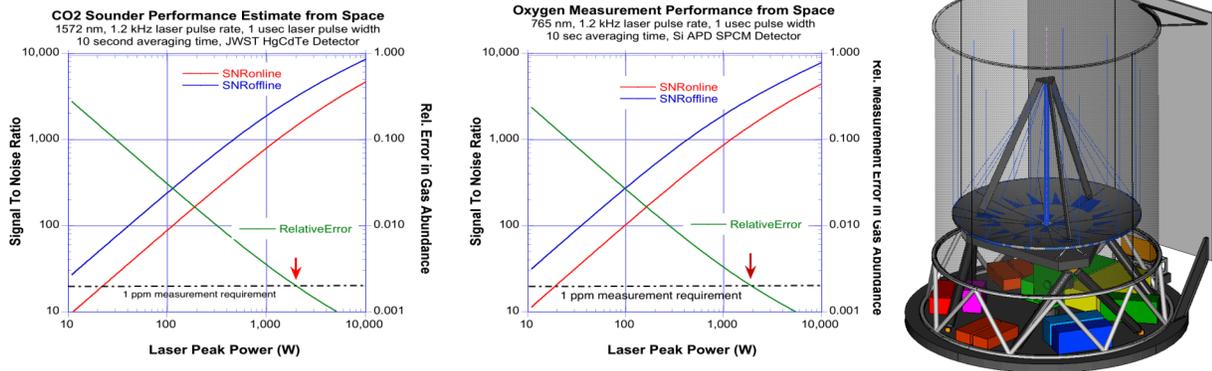


Figure 9 – Space lidar performance scaling and a lidar configuration for a 500 km orbit altitude. *Left* – Calculations for the CO₂ measurement SNR and relative error in column abundance vs laser peak power, for an assumed 1 usec laser pulse width, 10 sec of averaging time, based on receiver using a 1.5 m receiver diameter telescope and cooled HgCdTe APD detector. About 3 mJ/pulse is required, allowing for 3 dB margin. Similar performance can be achieved from a 450 km orbit with a NIR photomultiplier detector for the CO₂ measurement. *Middle* – A similar calculation for the O₂ measurement, assuming the receiver uses Si SPCM detectors, showing about the same energy is required with 3 dB margin. *Right* – The results of the initial space lidar study, showing a possible lidar configuration. Some elements shown are the 1.5 m receiver telescope, the radiator panel on the right, and most components mounted under the telescope’s primary mirror.

The instrument size is determined by the 1.5 m receiver telescope and the size of the thermal radiator. The instrument power consumption is between 600 and 900W depending on the CO₂ detector choice and its sensitivity. An initial mass estimate was about 400 kg, and the uncompressed data rate was < 2 Mbits/sec. The primary thermal sources were the laser amplifier stages. The instrument's volume and mass fit comfortably within the capabilities of medium-sized rocket assuming a nominal spacecraft. Although more work is needed based using better-defined measurement requirements and lidar components, the studies found no major space instrument design concerns.

10. SUMMARY

We have developed a technique and demonstrated airborne measurements of CO₂ absorption and column abundance using a pulsed direct detection lidar based on the IPDA technique. The lidar operates by stepping its laser wavelength across a CO₂ line near 1572 nm. For space 8 wavelengths are planned and the line scan frequency is 1 Khz. The direct detection receiver measures the time resolved backscatter and absorption line shape in the column to the surface. The time resolved measurement approach allows CO₂ column measurements through thin clouds.

We demonstrated airborne lidar measurements during summer 2009 during flights between 3-13 km altitudes. Measurements were made using the 1572.33 nm CO₂ line in flights over several locations and some through cirrus clouds. They showed clear absorption line shapes, which increased in optical depth with increasing aircraft altitude. The instrument's line shapes were estimated via a CO₂ line shape retrieval algorithm, which permitted solving and correcting for known instrument factors. The post-processed line shapes agreed well with ones calculated from in-situ measurements and radiosondes.

We have since made several improvements to the airborne lidar. We have improved the instrument's optical transmission, calibrations and receiver SNR. We have made additional flights on the NASA DC-8 during July 2010, to 13 km altitude, over various sites. We have also demonstrated lidar measurements of O₂ column absorption over horizontal paths, and in July 2010 we demonstrated airborne O₂ column absorption measurements. Those measurements are being analyzed and will be reported in the future. This work shows progress with this candidate approach for the ASCENDS mission. However to meet the ASCENDS mission goals, further analysis of the measurement requirements, and improvements in calibration, precision, airborne stability, readout rate and laser power scaling are needed. These are being addressed in ongoing work.

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